FORM PTO-1390 (REV. 9-2001) U S DEPARTMENT OF COMMERCE PATENT AND TRADEMARK OFFICE

TRANSMITTAL LETTER TO THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US) CONCERNING A FILING UNDER 35 U.S.C. 371

ATTORNEY 'S DOCKET NUMBER: **29462-032**

U.S. APPLICATION NO. (If known, see 37 CFR 1.5): **10/019326**

INTERNATIONAL APPLICATION NO.	INTERNATIONAL FILING DATE	PRIORITY DATE CLAIMED
PCT/EP00/04961	**31 May 2000**	**25 June 1999**

TITLE OF INVENTION: **AUSTENITIC Ni-Cr-Mo-Fe ALLOY**

APPLICANT(S) FOR DO/EO/US: **Ulrich BRILL, et al.**

Applicant herewith submits to the United States Designated/Elected Office (DO/EO/US) the following items and other information:

1. [X] This is a **FIRST** submission of items concerning a filing under 35 U.S.C. 371.
2. [ ] This is a **SECOND** or **SUBSEQUENT** submission of items concerning a filing under 35 U.S.C. 371.
3. [X] This is an express request to begin national examination procedures (35 U.S.C. 371(f)). The submission must include items (5), (6), (9) and (21) indicated below.
4. [ ] The US has been elected by the expiration of 19 months from the priority date (Article 31).
5. [X] A copy of the International Application as filed (35 U.S.C. 371(c)(2))
   a. [X] is attached hereto (required only if not communicated by the International Bureau).
   b. [X] has been communicated by the International Bureau.
   c. [ ] is not required, as the application was filed in the United States Receiving Office (RO/US).
6. [X] An English language translation of the International Application as filed (35 U.S.C. 371(c)(2)).
   a. [X] is attached hereto.
   b. [ ] has been previously submitted under 35 U.S.C. 154(d)(4).
7. [ ] Amendments to the claims of the International Aplication under PCT Article 19 (35 U.S.C. 371(c)(3))
   a. [ ] are attached hereto (required only if not communicated by the International Bureau).
   b. [ ] have been communicated by the International Bureau.
   c. [ ] have not been made; however, the time limit for making such amendments has NOT expired.
   d. [ ] have not been made and will not be made.
8. [ ] An English language translation of the amendments to the claims under PCT Article 19 (35 U.S.C. 371 (c)(3)).
9. [X] An oath or declaration of the inventor(s) (35 U.S.C. 371(c)(4)).
10. [ ] An English lanugage translation of the annexes of the International Preliminary Examination Report under PCT Article 36 (35 U.S.C. 371(c)(5)).

Items 11 to 20 below concern document(s) or information included:

11. [X] An Information Disclosure Statement under 37 CFR 1.97 and 1.98.
12. [X] An assignment document for recording. A separate cover sheet in compliance with 37 CFR 3.28 and 3.31 is included.
13. [X] A FIRST preliminary amendment.
14. [ ] A SECOND or SUBSEQUENT preliminary amendment.
15. [ ] A substitute specification.
16. [ ] A change of power of attorney and/or address letter.
17. [ ] A computer-readable form of the sequence listing in accordance with PCT Rule 13ter.2 and 35 U.S.C. 1.821 - 1.825.
18. [ ] A second copy of the published international application under 35 U.S.C. 154(d)(4).
19. [ ] A second copy of the English language translation of the international application under 35 U.S.C. 154(d)(4).
20. [X] Other items or information:
    PCT International Search Report (in German and English)
    International Preliminary Examination Report
    Express Mail Label No. EL616646561US

U.S. APPLICATION NO (if known, see 37 CFR)	INTERNATIONAL APPLICATION NO	ATTORNEY'S DOCKET NUMBER
10/019326	PCT/EP00/04961	29462-032

21. ☒ The following fees are submitted:	CALCULATIONS PTO USE ONLY	
BASIC NATIONAL FEE (37 CFR 1.492 (a) (1) - (5)):		
Neither international preliminary examination fee (37 CFR 1.482) nor international search fee (37 CFR 1.445(a)(2)) paid to USPTO and International Search Report not prepared by the EPO or JPO **$1040.00**		
International preliminary examination fee (37 CFR 1.482) not paid to USPTO but International Search Report prepared by the EPO or JPO **$890.00**		
International preliminary examination fee (37 CFR 1.482) not paid to USPTO but international search fee (37 CFR 1.445(a)(2)) paid to USPTO **$740.00**		
International preliminary examination fee (37 CFR 1.482) paid to USPTO but all claims did not satisfy provisions of PCT Article 33(1)-(4) **$710.00**		
International preliminary examination fee (37 CFR 1.482) paid to USPTO and all claims satisfied provisions of PCT Article 33(1)-(4) **$100.00**		
ENTER APPROPRIATE BASIC FEE AMOUNT =	$ 890.00	
Surcharge of **$130.00** for furnishing the oath or declaration later than ☐ 20 ☐ 30 months from the earliest claimed priority date (37 CFR 1.492(e)).	$	

CLAIMS	NUMBER FILED	NUMBER EXTRA	RATE		
Total claims	12 - 20 =	0	x $18.00	$	
Independent claims	1 - 3 =	0	x $84.00	$	
MULTIPLE DEPENDENT CLAIM(S) (if applicable)			+ $280.00	$	
TOTAL OF ABOVE CALCULATIONS =				$ 890.00	
☐ Applicant claims small entity status. See 37 CFR 1.27. The fees indicated above are reduced by 1/2. +				$ -	
SUBTOTAL =				$ 890.00	
Processing fee of **$130.00** for furnishing the English translation later than ☐ 20 ☐ 30 months from the earliest claimed priority date (37 CFR 1.492(f)).				$	
TOTAL NATIONAL FEE =				$ 890.00	
Fee for recording the enclosed assignment (37 CFR 1.21(h)). The assignment must be accompanied by an appropriate cover sheet (37 CFR 3.28, 3.31). **$40.00** per property +				$ 40.00	
TOTAL FEES ENCLOSED =				$ 930.00	
				Amount to be refunded:	$
				charged:	$

a. ☐ A check in the amount of $ _____ to cover the above fees is enclosed.

b. ☒ Please charge my Deposit Account No. **16-2500** in the amount of $ **930.00** to cover the above fees. A duplicate copy of this sheet is enclosed.

c. ☒ The Commissioner is hereby authorized to charge any additional fees which may be required, or credit any overpayment to Deposit Account No. **16-2500**. A duplicate copy of this sheet is enclosed.

d. ☐ Fees are to be charged to a credit card. **WARNING:** Information on this form may become public. **Credit card information should not be included on this form.** Provide credit card information and authorization on PTO-2038.

NOTE: Where an appropriate time limit under 37 CFR 1.494 or 1.495 has not been met, a petition to revive (37 CFR 1.137 (a) or (b)) must be filed and granted to restore the application to pending status.

SEND ALL CORRESPONDENCE TO:
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SIGNATURE

Charles Guttman
NAME

29,161
REGISTRATION NUMBER

Date: 21 December 2001

Attorney Docket No. : 29462-032

IN THE UNITED STATES DESIGNATED/ELECTED OFFICE (DO/EO/US)

Applicant	:	Ulrich BRILL, et al.
Int'l Appl. No.	:	PCT/EP00/04961
Int'l. Filing Date	:	May 31, 2000
Priority Date	:	June 25, 1999
Title of the Invention	:	AUSTENITIC Ni-Cr-Mo-Fe ALLOY

PRELIMINARY AMENDMENT

Assistant Commissioner for Patents
Box PCT
Washington, DC 20231

Express Mail Mailing Label No. :

EL616646561US

Sir:

Prior to examination, please amend the above-identified patent application as follows:

IN THE SPECIFICATION:

Page 1, after the title, please insert --BACKGROUND OF THE INVENTION--.

Page 3, before the first paragraph which begins with "It is the object," please insert --SUMMARY OF THE INVENTION--.

Page 3, before the paragraph, which begins with "This object is attained," please insert --DETAILED DESCRIPTION OF THE INVENTION--.

IN THE CLAIMS:

Please note that the claims have been amended in the International Application. In addition, please amend claims 3 to 12 of the amended claims to remove their multiple dependencies. A "marked-up" version of the amended claims is enclosed herewith in accordance with 37 C.F.R. 1.121 (c)(1).

--3. (Amended) Alloy as in claim 1, characterized in that the maximum total (in % by mass) of Al + Ti is 0.30.

--4. (Amended) Alloy as in claim 1, characterized in that the same scrap materials are used to produce the claimed alloy combination.

--5. (Amended) Alloy as in claim 1, characterized in that in particular three scrap materials with different mixture ratios are combined with each other.

--6. (Amended) Alloy as in claim 1, characterized in that an effective total WS = % Cr + 3[% Mo + 0.5 % W] + 16 % N ≥ 54 is selected.

--7. (Amended) Alloy as in claim 1, characterized in that a stretch limit $R_{p0,2}$ of at least 400 N/mm^2 is selected in the solution-annealed state.

--8. (Amended) Alloy as in claim 1, characterized in that a combination of WS≥ 54 with $R_{p0,2} \geq 400$ N/mm^2 is selected in the solution-annealed state.

--9. (Amended) Utilization of the alloy as in claim 1 as a welding additive material in the offshore industry, in particular for connection welding of longitudinal-seam pipes made of 6-Mo steel, duplex and super-duplex steel.

--10. (Amended) Utilization of the alloy as in claim 1 as additive welding material for build-up welding, in particular for flanges in the offshore field, or for boiler pipes in waste burning plants.

11. (Amended) Utilization of the alloy as in claim 1 as a build-up welding band in plant construction.

12. (Amended) Utilization of the alloy as in claim 1 in gas channels of flue gas desulphurization installations.

REMARKS

Amendments are being made to claims 3-12 to remove their multiple dependencies.

Please proceed to examine the application as amended herein.

Respectfully submitted,
PROSKAUER ROSE LLP
Attorneys for Applicant(s)

Date: December 21, 2001

By _____
Charles Guttman
Reg. No. 29,161

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Amended Claims - Marked-Up Version

3. Alloy as in claim 1 [or 2], characterized in that the maximum total (in % by mass) of Al + Ti is 0.30.

4. Alloy as in [one of the claims 1 to 3] claim 1, characterized in that the same scrap materials are used to produce the claimed alloy combination

5. Alloy as in [one of the claims 1 to 4] claim 1, characterized in that in particular three scrap materials with different mixture ratios are combined with each other.

6. Alloy as in [one of the claims 1 to 5] claim 1, characterized in that an effective total WS = % Cr + 3[% Mo + 0.5 % W] + 16 % N ≥ 54 is selected.

7. Alloy as in [one of the claims 1 to 6] claim 1, characterized in that a stretch limit $R_{p0,2}$ of at least 400 N/mm^2 is selected in the solution-annealed state.

8. Alloy as in [claims 1 to 7] claim 1, characterized in that a combination of WS≥ 54 with $R_{p0,2} \geq 400$ N/mm^2 is selected in the solution- annealed state.

9. Utilization of the alloy as in [one of the claims 1 to 8] claim 1 as a welding additive material in the offshore industry, in particular for connection welding of longitudinal-seam pipes made of 6-Mo steel, duplex and super-duplex steel.

10. Utilization of the alloy as in [one of the claims 1 to 8] claim 1 as additive welding material for build-up welding, in particular for flanges in the offshore field, or for boiler pipes in waste burning plants.

11. Utilization of the alloy as in [one of the claims 1 to 8] claim 1 as a build-up welding band in plant construction.

12. Utilization of the alloy as in [one of the claims 1 to 8] claim 1 in gas channels of flue gas desulphurization installations.

Austenitic Ni-Cr-Mo-Fe Alloy

The invention relates to an austenitic warm or cold-formable alloy.

Until now austenitic, austenitic-ferritic, ferritic as well as ferritic-martensitic steel on the one hand, and on the other hand nickel based alloys were used until now as materials for mechanical and at the same time chemically corrosion resistant components under heavy stress. The mechanical strength of austenitic steel is not sufficient for several applications. With ferritic-austenitic steel as well as with ferritic and ferritic-martensitic steel its poor processing behavior (hot forming, weldability) and the insufficient corrosion resistance are disadvantages.

EP-B1 0 334 410 has disclosed a nickel-chrome-molybdenum alloy that contains (by % of mass) the following alloy elements:

22.0 to 24.0 chrome
15.0 to 16.5 molybdenum
Up to 0.3 wolfram
Up to 1.5 iron
Up to 0.3 cobalt
Up to 0.1 silicon
Up to 0.5 manganese
up to 0.015 carbon
up to 0.4 vanadium
0.1 to 0.4 aluminum
0.001 to 0.4 magnesium
0.001 to 0.04 calcium

The residue consists of nickel and includes and unavoidable impurities.

EP-B1 0 247 577 has disclosed an ally on nickel basis containing chrome and molybdenum which can be hardened and containing, (in % by mass) the following alloy components:

Carbon max. 0.1
Manganese max. 5
Silicon max 1
Phosphor max 0.03
Sulfur max 0.03
Chrome 16-24
Molybdenum 7 to 12
Niobium 2 to 6
Titanium 0.50 to 2.5
Traces of aluminum up to 1
Boron max. 0.02
Zirconium max. 0.050
Cobalt max. 5
Copper max. 5

and containing in addition at least 50% nickel as residue as well as impurities due to production, with the total of chrome and molybdenum no greater than 31 and the total of niobium, titanium and aluminum is such that their total atomic weight percentage comes to 3.5 to 5 and combines in solution annealed and hardened form a 0.2% stretch limit of over 100 ksi (690 MN/m^2) combined with a resistance to fissure corrosion and crevice

corrosion as well as against tension fissure corrosion in a chloride and sulfide environment at high temperature up to 260°C without requiring work below its recrystallization temperature.

If extreme corrosion conditions exist, it is necessary in many areas of application to have recourse to comparatively expensive Ni-Cr-Mo alloys with Fe contents limited in part to a maximum of 1%. But the alloys established on the market still are no longer sufficient to meet all requirements in today's chemical and petrochemical process technology, nor in the present environmental protection technology, in particular when at the same time high tensile limits or tensible strength are required. Problems often occur when known alloys are used as welding additives, in particular in the field of offshore technology, where mostly 6-Mo steel, duplex and super-duplex steel is welded.

It is the object of the present invention to propose an alloy that can be used in particular under extreme corrosive conditions and possesses at the same time extraordinarily high tensile limits and tensible strength. The alloy must possess high resistance to crevice and fissure corrosion as well as to removing corrosion and it must furthermore be possible to produce and process it without problems. For this reason the required strength of the alloy must already exist in the solution annealed or soft annealed state, so that additional hardening and heat treatment can be dispensed with.

This object is attained with an austenitic alloy which can be hot and cold-formed for use in aqueous, oxidizing media, consisting of the following alloy elements (in % by mass):

Cr	18.0-21.0
Fe	12.0-16.0
Mo	9.0-13.0
Co	max. 1.0
W	0.5-2.5
C	max. 0.025
N	0.05-0.25
Mn	max. 0.50
Si	max. 0.50
Ti	max. 0.02
Nb	0.05-0.5
Cu	max. 0.3
P	max. 0.010
Al	0.05-0.5
S	max. 0.005
Mg	0.005-0.030
Ca	0.001-0.01
V	max. 0.5
B	max. 0.005
Zr	0.001-0.030

The residue consists of nickel and includes impurities resulting from production.

An especially preferred alloy is composed of the following alloy elements (in % by mass):

Cr	19.0-20.0
Fe	13.0-15.0
Mo	10.0-12.0
Co	max. 1.0
W	1.0-2.0
C	max. 0.025
N	0.05-0.15
Mn	max. 0.50
Si	max. 0.50
Ti	max. 0.02
Nb	0.1-0.3

Cu	max. 0.3
P	max. 0.010
Al	0.10-0.35
S	max. 0.005
Mg	0.006-0.020
Ca	0.001-0.005
V	max. 0.30
B	max. 0.002
Zr	0.005-0.025

The residue consists of nickel and includes impurities resulting from production.

The total contents of aluminum + titanium are preferably limited to 0.30 (in % by mass). The same applies to the total contents of niobium + tantalate which are also kept at 0.30 (in % by mass).

Raising the iron content of the alloy according to the invention to 13 to 15 (in % by mass) results on the one hand in improved workability and formability, and on the other hand also to a considerable reduction of costs due to the lower met al price and the lowering of production costs. Contrary to generally held belief that less than 1% iron content is needed for build-up welding with Ni-Cr-Mo alloys on non-alloyed or low-alloyed steel, i.e. that a mixing up of iron in the welding deposit is prevented to a great extent, comparative investigations of the alloy A according to the invention and of the comparison alloy B which were used as welding additives for one- and two-layered build-up welding on St 52, shows that the iron content of the build-up welding carried out with the ally A according to the invention is even lower than with the build-up welding with the comparison alloy B. This is shown in Fig. 1.

Elements	1-layered		2-layered	
	Alloy A	Alloy B	Alloy A	Alloy B
Ni	Residue	30	Residue	41.5
Cr	12.2	11	16.5	14.5
Mo	6.55	4.2	9.1	6
Fe	47.9	52.5	28.1	35
W	0.75	n.b.	1.13	n.b

Fig. 1: Chemical analyses of the build-up welding with the alloy A according to the invention and of the comparison alloy B on St 52.

The chemical composition (% by mass) of the comparison alloy B is as follows:

Cr	22
Fe	3.0
C	0.025
Mn	0.40
Si	0.40
Mo	8.0
Co	1.0
Al	0.40
Ti	0.40
Nb	3.5
P	0.010
S	0.010

Lowering the niobium content of the alloy A according to the invention to (in % by mass) preferably 0.1 to 0.3 results in far better weldability than with the comparison alloy B.

In addition a faultless and sediment-free, high-load bearing weld connection with duplex and super duplex steel having high nitrogen contents becomes at all possible.

Increasing the molybdenum content of the alloy A according to the invention to (in % by mass) 10 to 12, as well as increasing the W content to (in % by mass) 1 to 2 results in greater crevice and fissure corrosion resistance than alloy B, as is documented in Fig. 2.

Contrary to the instruction incorporated in EP-B1 0 247 577, according to which nitrogen contents up to 0.04% are acceptable and no precise specifications are given concerning the influence of nitrogen, the investigation of the influence of nitrogen in the alloy A according to the invention shows that nitrogen clearly increases the tensile limits and tensible strength on the one hand, and on the other hand clearly improves the corrosion resistance of the alloy A according to the invention. Fig. 3 shows this as an example of tensible strength Rm over nitrogen content, and Fig. 4 shows the tensible strength $R_{p0.2}$ over the nitrogen content for the alloy A according to the invention. The tensile limit is increased by approximately 30 % and the tensible strength by approximately 20 %.

The increase of the crevice corrosion resistance of the alloy according to the invention thanks to the addition of nitrogen is clearly shown in Fig. 5. In the state of the art, the crevice corrosion resistance is determined according to ASTM G48, method D, as well as "Green Death" solution (7% H_2S0_4, 3% HCl, 1% $FeCl_3$, 1% $CuCl_2$). The critical crevice corrosion temperature increases in both tests as the content in nitrogen increases.

The alloy according to the present invention finds its application as an additive welding material in the offshore industry, in particular for connecting welding of long-seam welded pipes made of 6-Mo steel, duplex and super-duplex steel.

In addition, the possibility exists to utilize the alloy according to the invention as a welding additive material for build-up welding, in particular for flanges in the offshore field or for boiler pipes in waste burning plants.

Finally it is also possible to use the alloy according to the invention as a build-up welding band in plant construction and in addition to use it in gas channels of flue gas desulphuration installations.

In an extension of the invention, the alloy according to the invention can be obtained by melting scrap alloy combinations so that the narrow margins of the different alloy elements defined in the claims are implemented.

CLAIMS

1. Austenitic alloy which can be hot and cold-formed for use in aqueous, oxidizing media containing chloride, consisting of the following alloy elements (in % by mass):

Cr	18.0-21.0
Fe	12.0-16.0
Mo	9.0-13.0
Co	max. 1.0
W	0.5-2.5
C	max. 0.025
N	0.05-0.25
Mn	max. 0.50
Si	max. 0.50
Ti	max. 0.02
Nb	0.05-0.5
Cu	max. 0.3
P	max. 0.010
Al	0.05-0.5
S	max. 0.005
Mg	0.005-0.030
Ca	0.001-0.01
V	max. 0.5
B	max. 0.005
Zr	0.001-0.030

Nb and Ta as needed, with the total of Nb and Ta being at most 0.30.

The residue consists of nickel and includes impurities resulting from production.

2. Alloy as in claim 1, characterized by the following alloy elements (% by mass)

Cr	19.0-20.0
Fe	13.0-15.0
Mo	10.0-12.0
Co	max. 1.0
W	1.0-2.0
C	max. 0.020
N	0.05-0.15
Mn	max. 0.50
Si	max. 0.50
Ti	max. 0.02
Nb	0.1-0.3
Cu	max. 0.3
P	max. 0.010
Al	0.10-0.35
S	max. 0.005
Mg	0.006-0.020
Ca	0.001-0.005
V	max. 0.30
B	max. 0.002
Zr	0.005-0.025

The residue consists of nickel and includes impurities resulting from production.

3. Alloy as in claim 1 or 2, characterized in that the maximum total (in % by mass) of Al + Ti is 0.30.

4. Alloy as in one of the claims 1 to 3, characterized in that the same scrap materials are used to produce the claimed alloy combination

5. Alloy as in one of the claims 1 to 4, characterized in that in particular three scrap materials with different mixture ratios are combined with each other.

6. Alloy as in one of the claims 1 to 5, characterized in that an effective total WS = % Cr + 3[% Mo + 0.5 % W] + 16 % N ≥ 54 is selected.

7. Alloy as in one of the claims 1 to 6, characterized in that a stretch limit $R_{p0,2}$ of at least 400 N/mm^2 is selected in the solution-annealed state.

8. Alloy as in claims 1 to 7, characterized in that a combination of WS≥ 54 with $R_{p0,2} \geq 400$ N/mm^2 is selected in the solution-annealed state.

9. Utilization of the alloy as in one of the claims 1 to 8 as a welding additive material in the offshore industry, in particular for connection welding of longitudinal-seam pipes made of 6-Mo steel, duplex and super-duplex steel.

10. Utilization of the alloy as in one of the claims 1 to 8 as additive welding material for build-up welding, in particular for flanges in the offshore field, or for boiler pipes in waste burning plants.

11. Utilization of the alloy as in one of the claims 1 to 8 as a build-up welding band in plant construction.

12. Utilization of the alloy as in one of the claims 1 to 8 in gas channels of flue gas desulphurization installations.

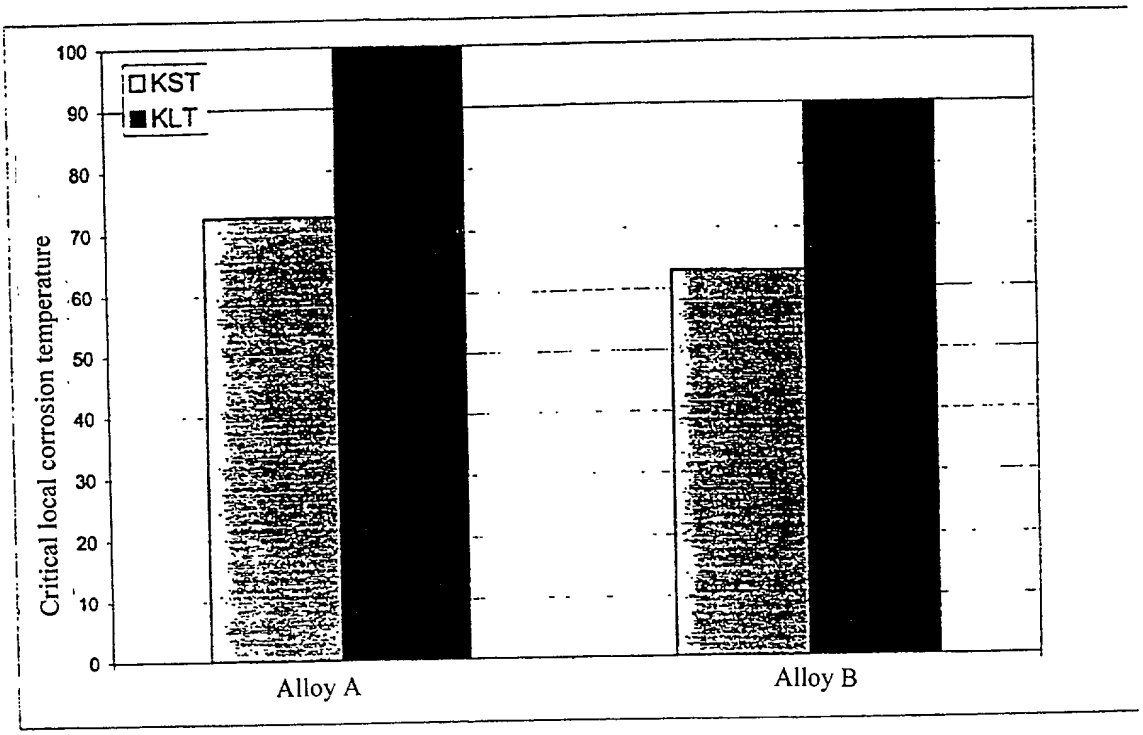

Fig. 2: Critical crevice and critical fissure corrosion temperature of the alloy A according to the invention and of the comparison alloy B following testing in "green death" solution (7% H_2S0_4, 3% HCl, 1% $FeCl_3$, 1% $CuCl_2$)

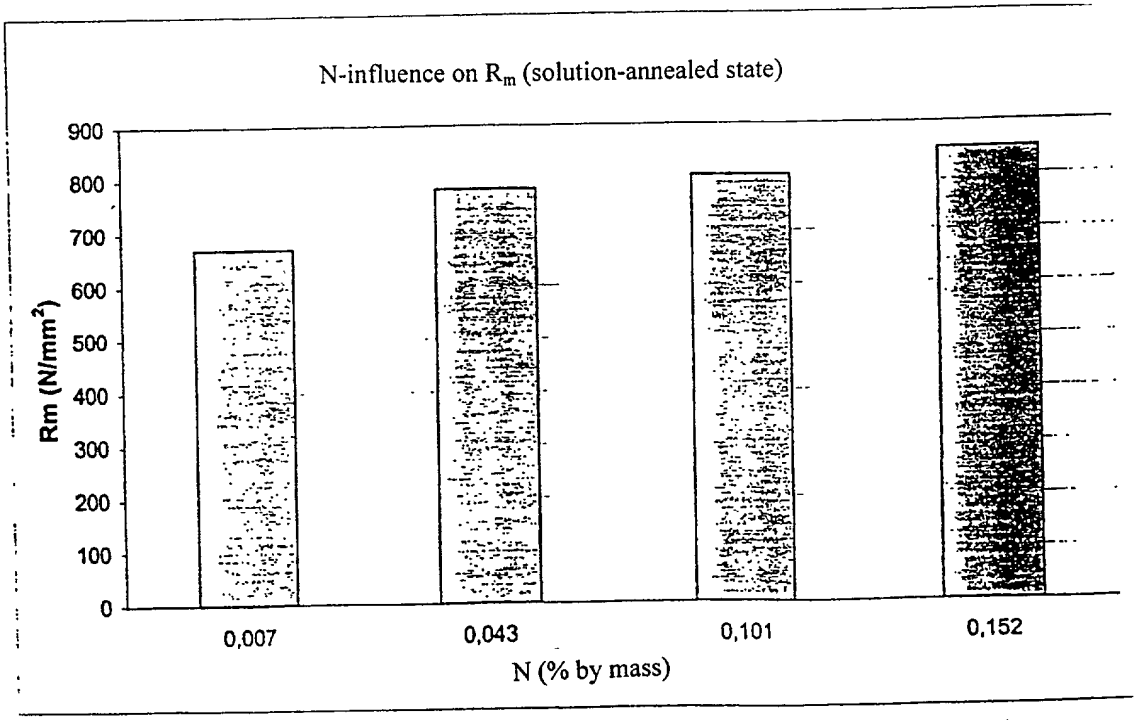

Fig. 3: Influence of nitrogen on the tensible strength of the alloy A according to the invention.

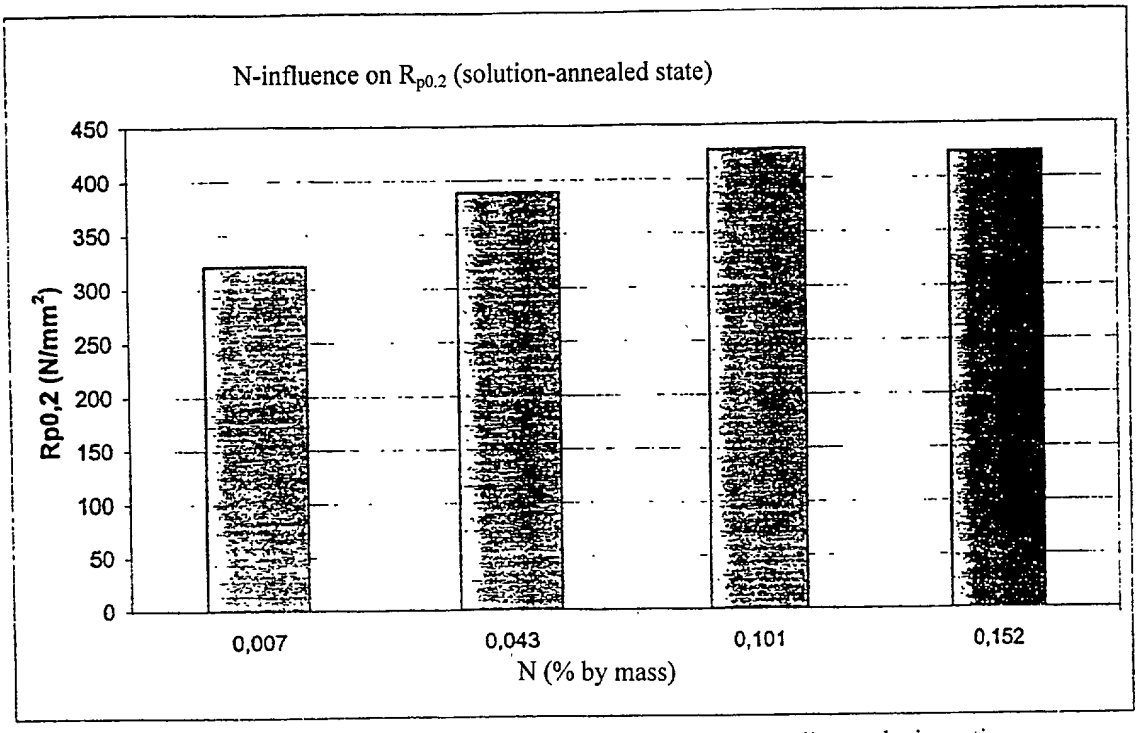

Fig. 4: Influence of nitrogen on the tensile limit of the alloy A according to the invention.

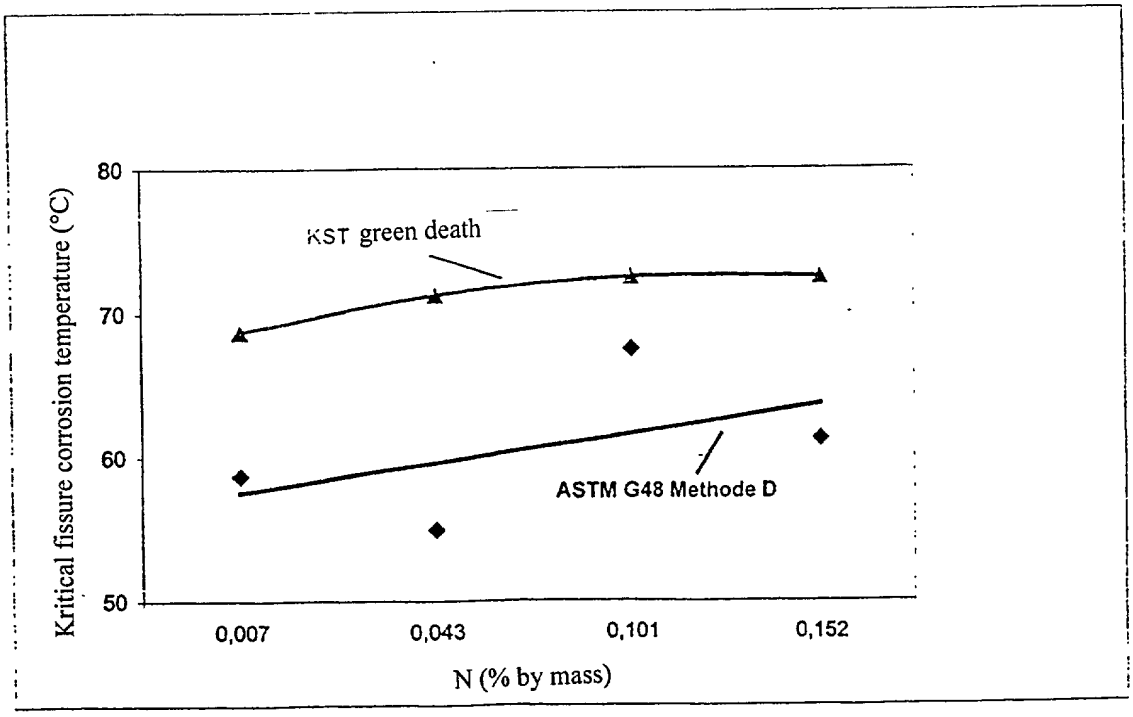

Fig. 3: Influence of nitrogen on the fissure corrosion resistance of the alloy A according to the invention (according to ASTM G 48, Method D, as well as in "Green death" (7% H_2S0_4, 3% HCl, 1% $FeCl_3$, 1% $CuCl_2$)

DECLARATION FOR PATENT APPLICATION

As a below named inventor, I hereby declare that:

My residence, post office address and citizenship are as stated below next to my name. I believe I am the original, first and sole inventor (if only one name is listed below) or an original, first and joint inventor (if plural names are listed below) of the subject matter which is claimed and for which a patent is sought on the invention entitled:

AUSTENITIC NI-CR-MO-FE ALLOY

the specification of which is attached hereto unless the following box is checked:

__X__ was filed on **May 31, 2000** as United States Application Number _____
or PCT International Application Number **PCT/EP00/04961**
and was amended on _____ (if applicable).

I hereby state that I have reviewed and understand the contents of the above identified specification, including the claims, as amended by any amendment referred to above. I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR § 1.56.

I hereby claim foreign priority benefits under 35 U.S.C. § 119(a) or § 365(b) of any foreign application(s) for patent or inventor's certificate, or § 365(a) of any PCT International application which designated at least one country other than the United States, listed below and have also identified, by checking the box, any foreign application for patent or inventor's certificate, or PCT International Application having a filing date before that of the application on which priority is claimed.

Prior Foreign Application(s)			Priority Not Claimed
199 29 354.6	Germany	25/6/1999	_____
(Number)	(Country)	(Day/Month/Year Filed)	
_____	_____	_____	_____
(Number)	(Country)	(Day/Month/Year Filed)	

I hereby claim the benefit under 35 U.S.C. § 119(e) of any United States provisional application(s) listed below.

(Application Number)	(Filing Date)
(Application Number)	(Filing Date)

I hereby claim the benefit under 35 U.S.C. § 120 of any United States application(s), or § 365(c) of any PCT International application designating the United States, listed below and, insofar as the subject matter of each of the claims of this application is not disclosed in the prior United States or PCT International application in the manner provided by the first paragraph of 35 U.S.C. § 112, I acknowledge the duty to disclose information which is material to patentability as defined in 37 CFR § 1.56 which became available between the filing date of the prior application and the national or PCT International filing date of this application.

(Application Number)	(Filing Date)	(Status--patented, pending, abandoned)
(Application Number)	(Filing Date	(Status--patented, pending, abandoned)

I hereby appoint the following attorney(s) and/or agent(s) to prosecute this application and to transact all business in the Patent and Trademark Office connected therewith:

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I hereby declare that all statements made herein of my own knowledge are true and that all statements made on information and belief are believed to be true; and further that these statements were made with the knowledge that willful false statements and the like so made are punishable by fine or imprisonment, or both, under Section 1001 of Title 18 of the United States Code and that such willful false statements may jeopardize the validity of the application or any patent issued thereon.

1-00

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